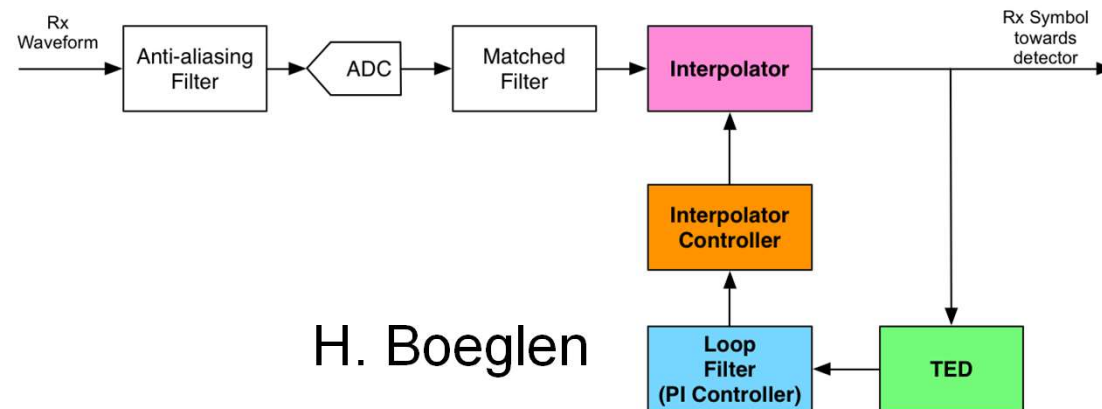




From a simulated to a real digital communication system: a QPSK modem design with GNU Radio



H. Boeglen

XLIM, UMR CNRS 6172, Université de Poitiers, France

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Outline

- 1 – Introduction and motivation
- 2 – QPSK modem: the main building blocks
- 3 – The fully digital QPSK synchronizer.
- 4 – GNU Radio demo with real hardware
- 5 – Conclusion

Outline

1 – Introduction and motivation

2 –

3 –

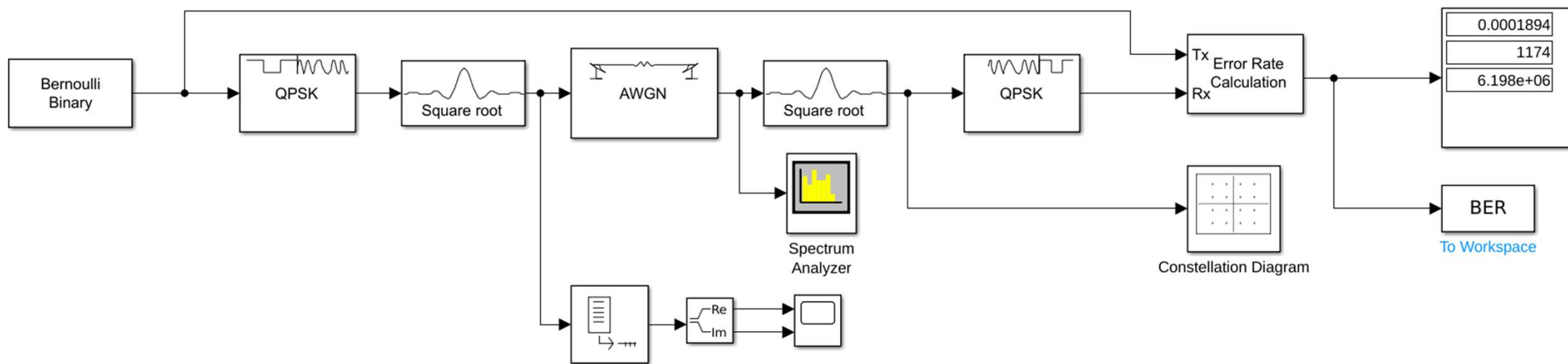
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5 –

1. Introduction & motivation

□ I have been teaching digital communications (DC) at undergraduate and graduate levels for more than 15 years.

□ Extensive use of Matlab/Simulink and the Communications toolbox:



➔ Very good tool to illustrate the main DC concepts by simulation.

- ❑ Up to this year in the 2nd year of the IoT master's degree two disjoint topics taught in the DC course:
 - ➔ Basics + ECC (me)
 - ➔ Hardware aspects: linearity in RF amplifiers (my colleague)
- ❑ Everything is taught using Matlab/Simulink simulation tools.
- ❑ My colleague has discovered the power of GNU Radio in a DPD (digital pre-distortion) research project.
- ❑ We have decided to give more coherence to the course by:
 - ➔ Replacing Matlab/Simulink by GNU Radio as much as possible (at last; I do not want to have trouble with JM 😊).

- **Giving more space to implementation with the design of a real world QPSK modem (GNU Radio + hardware (Adalm-Pluto) up to the linearized PA).**
- ❑ **So this presentation will be about the difficulties you'll face when you go from simulation to implementation!**
- ❑ **Since it is the topic of these 2 days we will focus mainly on synchronization aspects.**
- ❑ **Well, no choice: no synchronization means no real world implementation anyway.**

Outline

1 –

2 – QPSK modem: the main building blocks

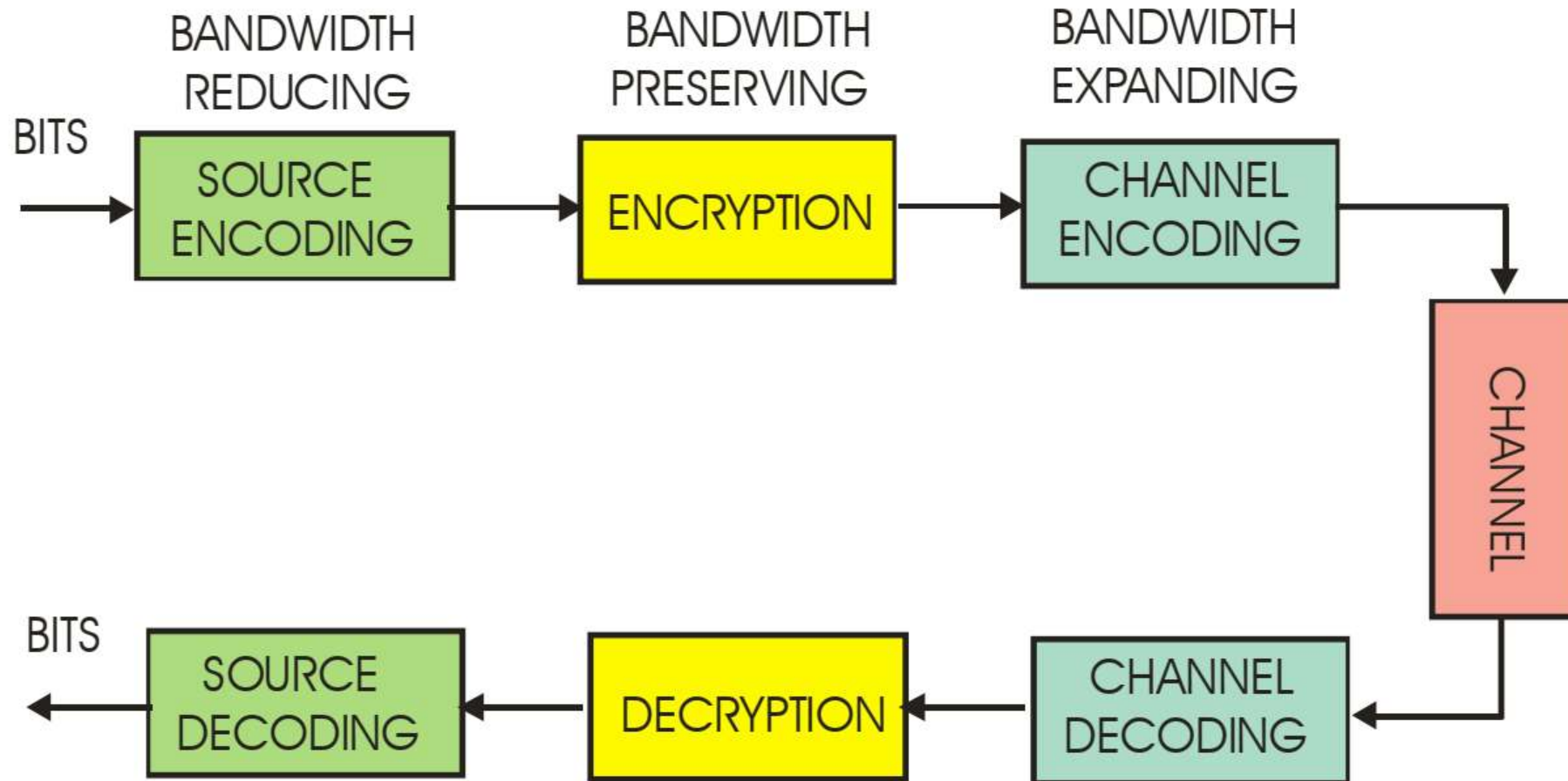
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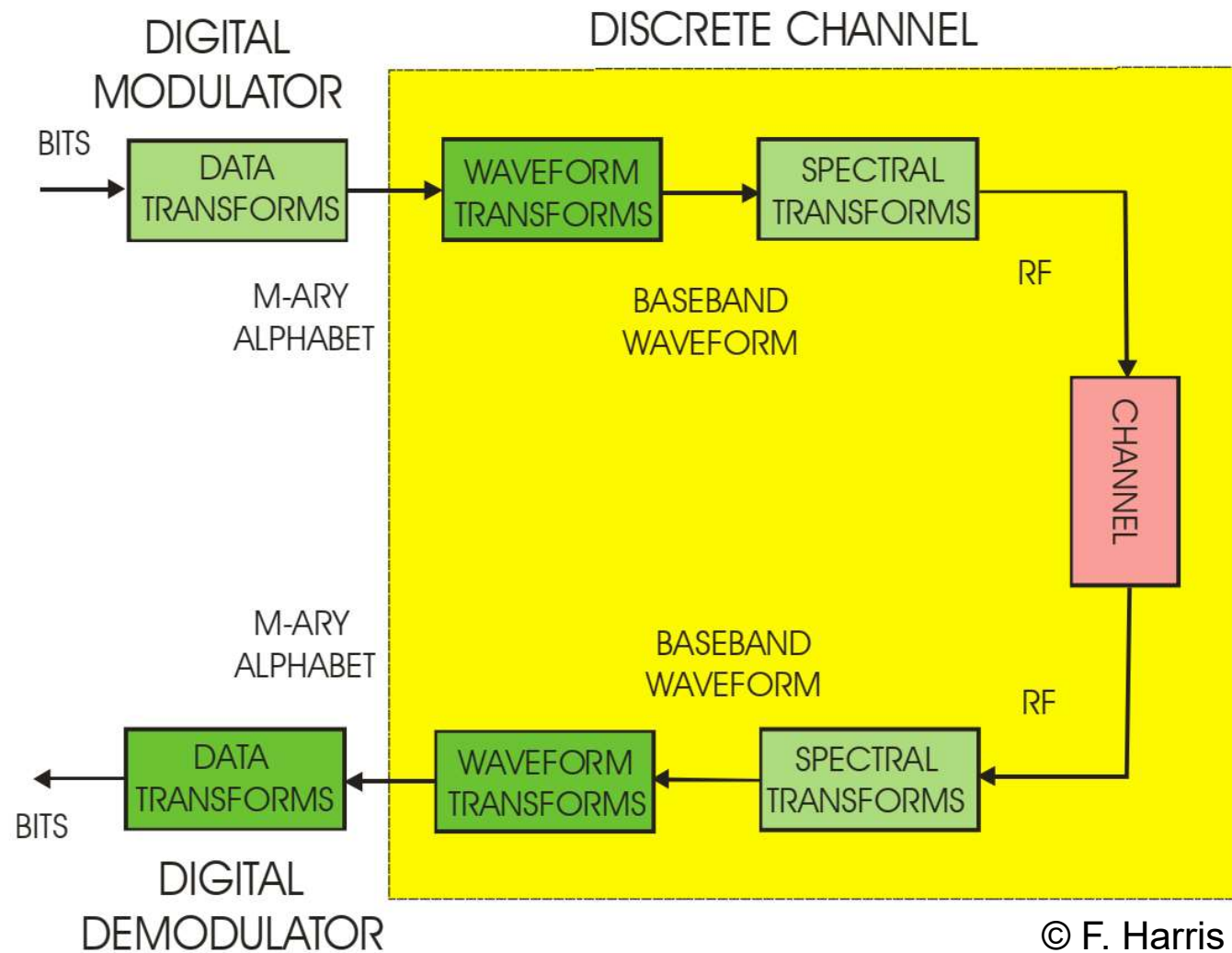
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2. QPSK modem: the main building blocks

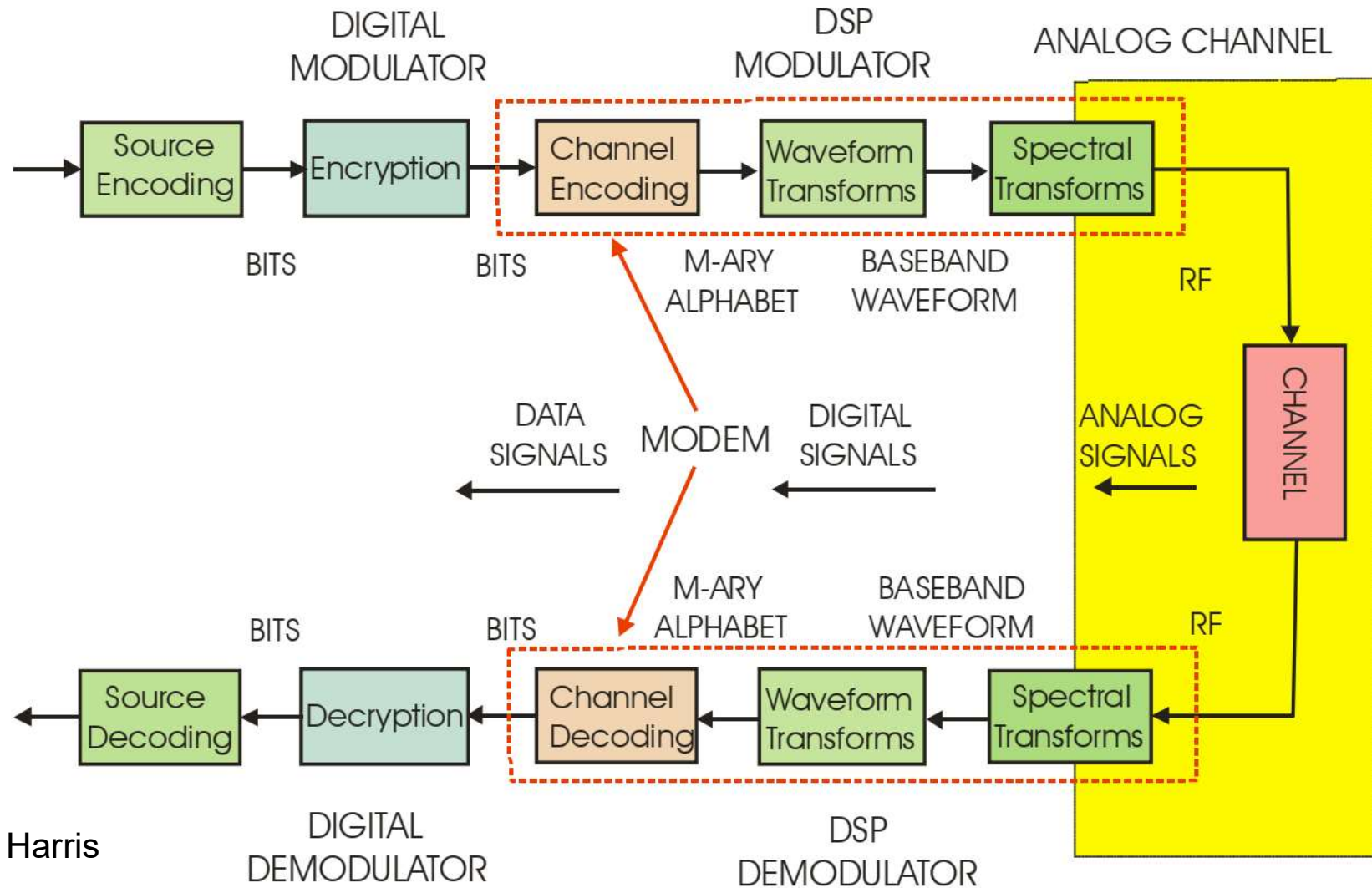
□ From Shannon to the digital QPSK modem



□ From Shannon to the digital QPSK modem

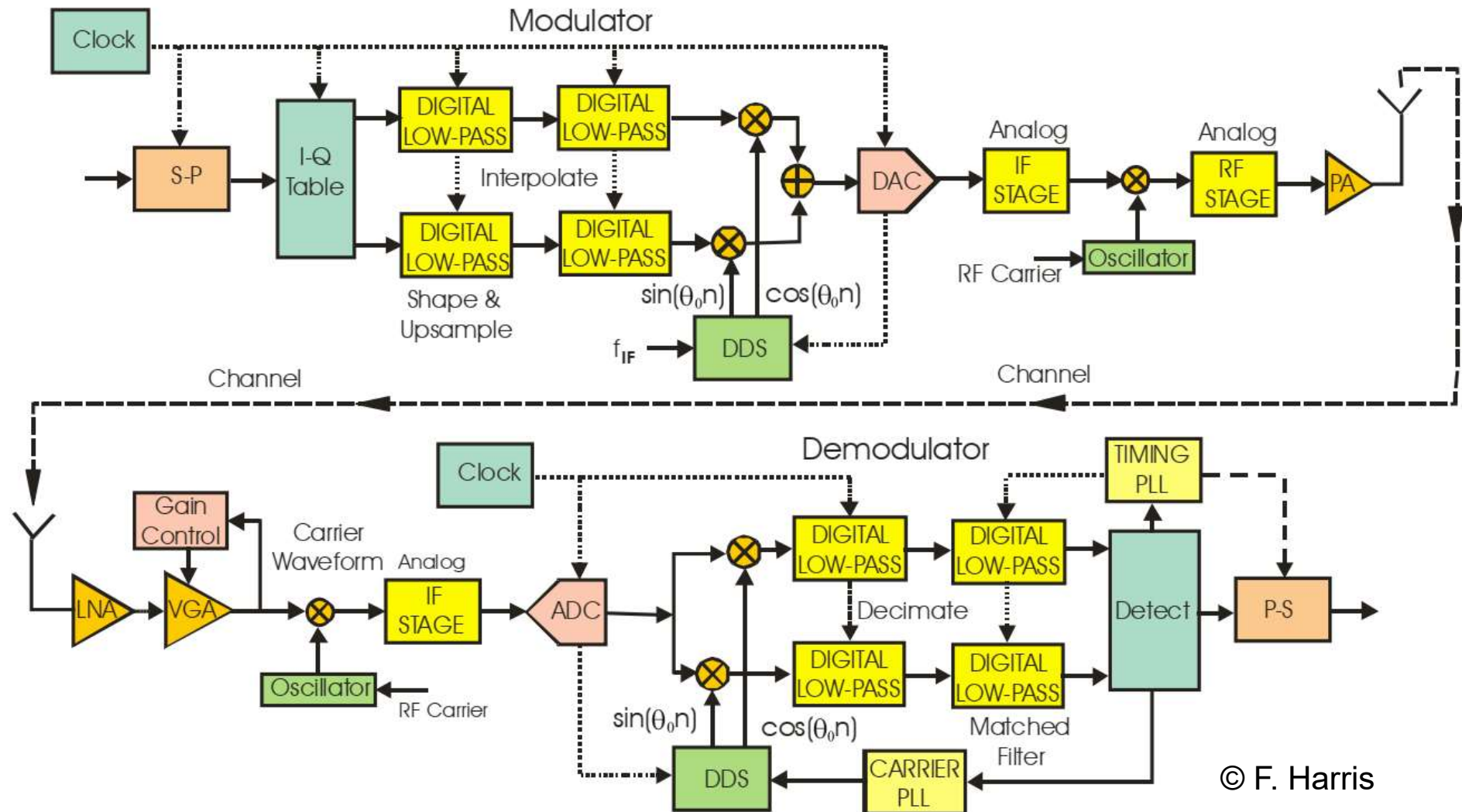


□ From Shannon to the digital QPSK modem



2. QPSK modem: the main building blocks

□ From Shannon to the digital QPSK modem



2. QPSK modem: the main building blocks

❑ Pulse shaping and matched filtering needed for:

→ Limiting the BW

→ Maximizing SNR at the decision points

→ Reduce ISI

❑ Use of the well known Root Raised Cosine (RRC) pulse

→ One at the transmitter and one at the receiver = Raised Cosine response, i.e. Nyquist ISI criterion.

❑ In practice: what are the important parameters?

→ Upsampling factor N (SPS): (4 to 16)

→ Filter span (number of symbols).

→ Roll-off α (excess bandwidth/cardinal sine): between 0.25 and 0.6.

2. QPSK modem: the main building blocks

□ RRC pulse filter coefficients generation

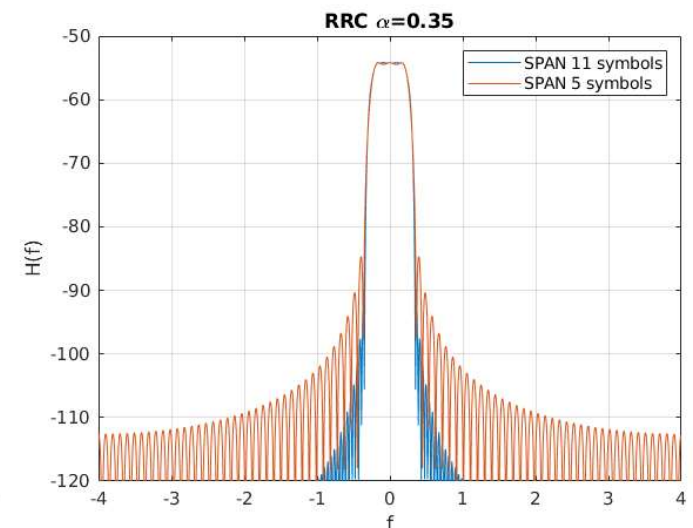
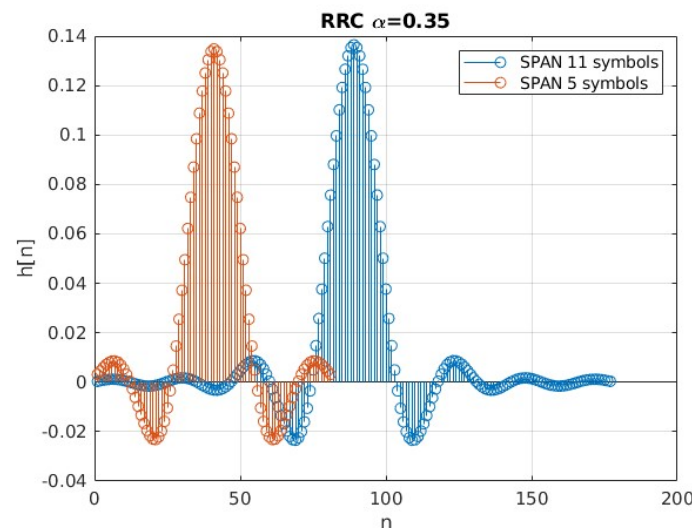
→ Matlab `h = rcosdesign(α , SPAN, SPS)`

→ Octave `h = rcosfir(α , nT, SPS, T, 'sqrt')`

→ GNU Radio `firdes.root_raised_cosine(gain, SPS, T, α , nTaps (SPAN*SPS))`

- RRC pulse filter example ($\alpha = 0.35$, SPS = 16, SPAN = 11)

`firdes.root_raised_cosine(2,
2*8, 1.0, 0.35, (11 or 5)*8*2)`



2. QPSK modem: the main building blocks

□ How many samples per symbol (N)?

$N = T_s/T$ with T_s = sample rate and T = symbol rate

In practice: $4 \leq N \leq 16$

□ Be careful about the signal level at the reception side!

- At baseband: system with symbol of unit energy.
- Amplitude A is then given by:

→ $A = \sqrt{(3 \cdot E_s)/(2 \cdot (M-1))}$ with E_s = symbol energy in J and M = number of points of the constellation.

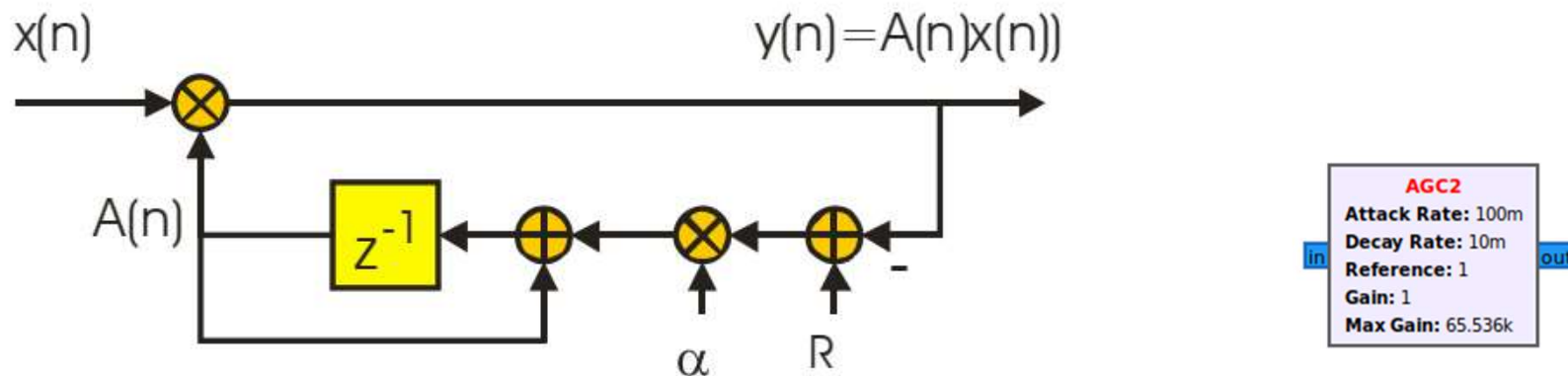
→ For QPSK $A = \sqrt{2.0} = 0.707$.

Receiver functions designed to handle this value which has to remain constant → need for an AGC

2. QPSK modem: the main building blocks

□ Signal level at the reception side: AGC

- Need to ensure a constant signal level for the receiver function to work
- Signal cannot be constant because propagation channel varies
- Use of an Automatic Gain Control (AGC) structure



$$A[n+1] = A[n](1-\alpha c) + \alpha R$$

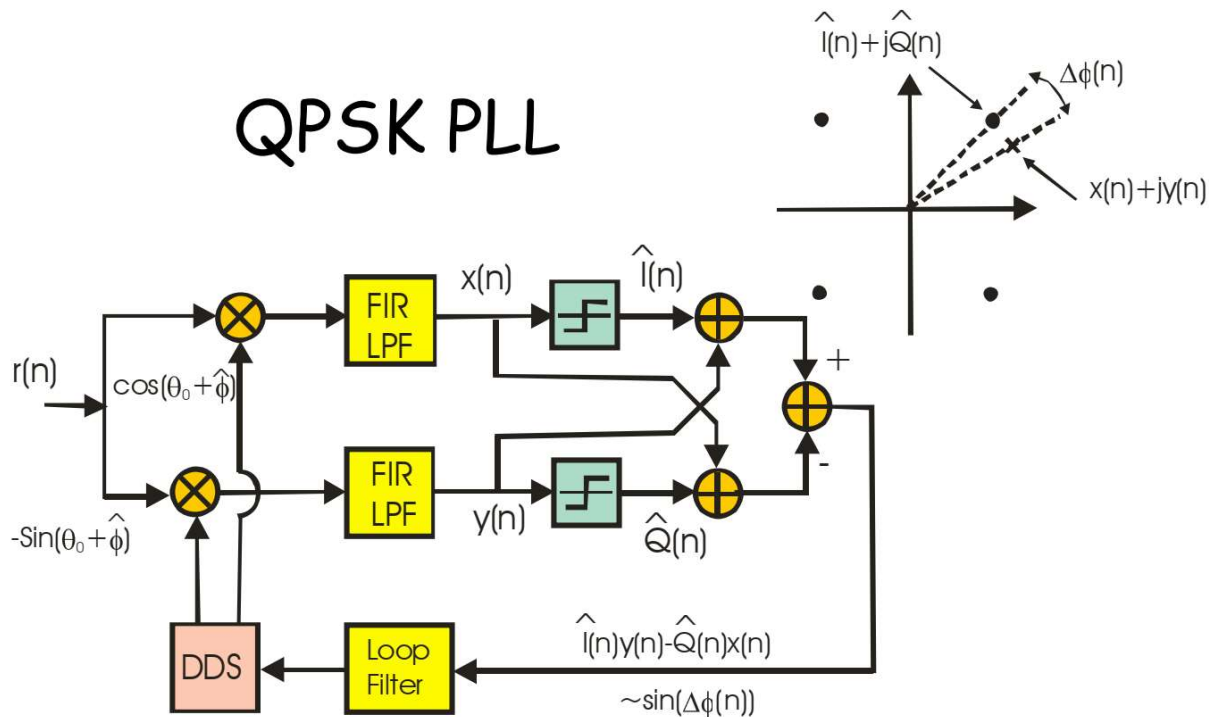
R = reference, α = gain c = constant and $\alpha c < 2.0$.

Loop time constant is $1/\alpha c$ samples.

If c small long transient. If c large short transient.

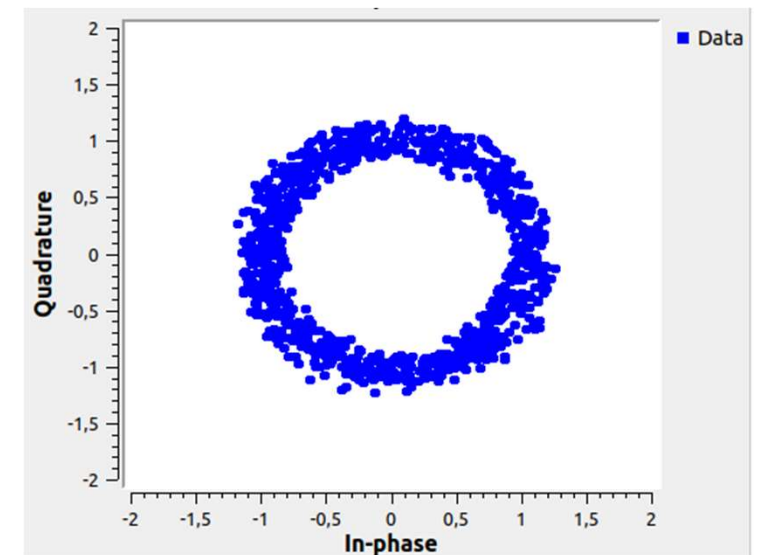
2. QPSK modem: the main building blocks

- Some more loops: carrier and timing synchronization PLLs
 - Carrier and phase recovery loop
 - TX oscillator unknown phase
 - Generated carrier frequency f_{RX} at receiver is not exactly f_{TX}



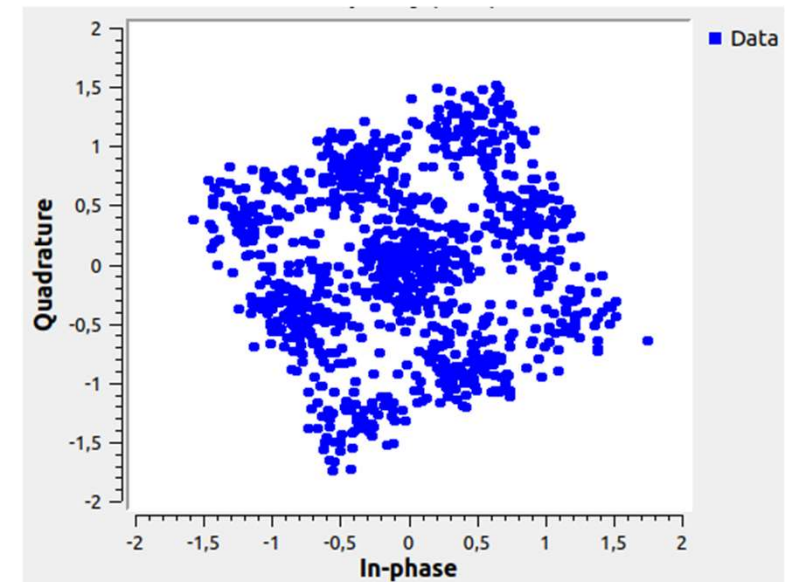
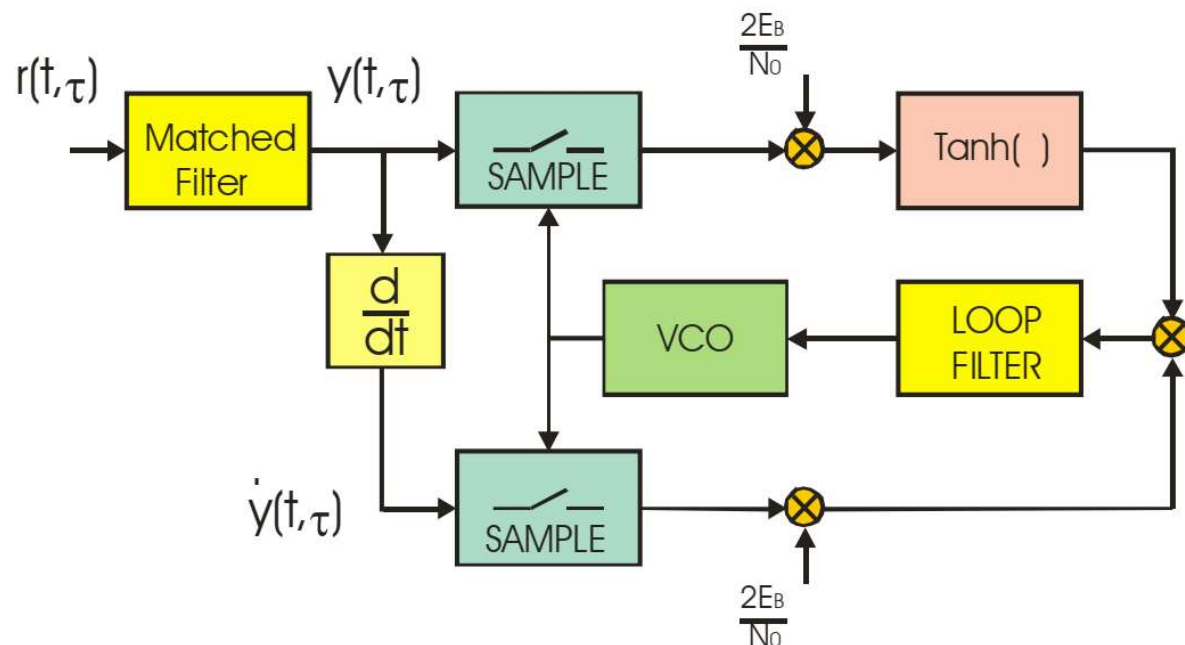
Direct Digital Synthesizer

Has a $\pi/2$ phase ambiguity!



2. QPSK modem: the main building blocks

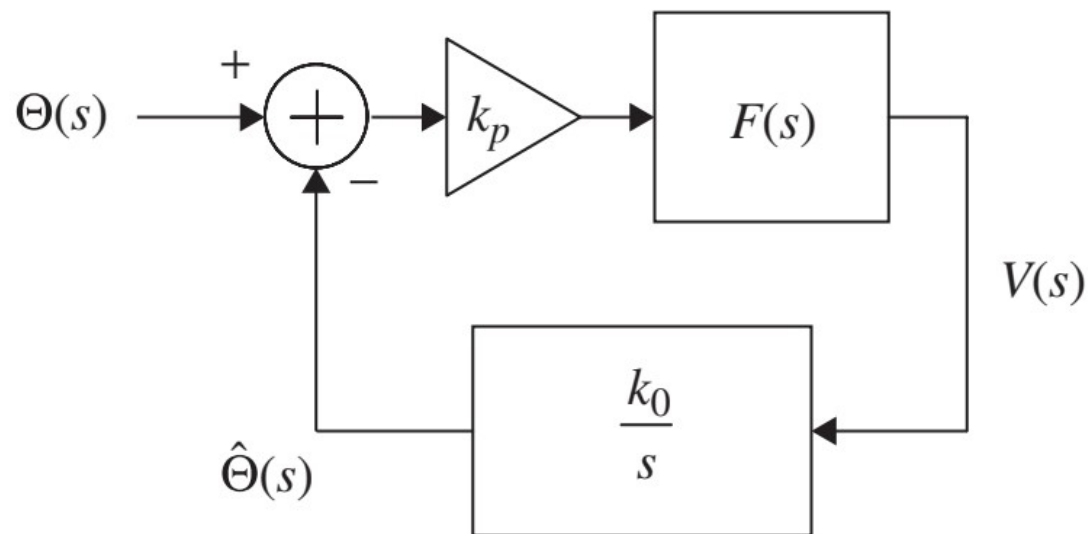
- ❑ Some more loops: carrier and timing synchronization PLLs
 - Timing recovery loop
 - ➔ Optimum sampling instants have to be extracted from the data



2. QPSK modem: the main building blocks

□ From analog PLL to digital PLL and its main parameters

- We will restrict to a second order loop (the most used).
- The analog PLL



Proportional-plus-integrator filter:

$$F(s) = k_1 + \frac{k_2}{s}$$

Transfer function:

$$H_a(s) = \frac{k_0 k_p k_1 s + k_0 k_p k_2}{s^2 + k_0 k_p k_1 s + k_0 k_p k_2}$$

Can be rewritten:

$$H_a(s) = \frac{2\zeta\omega_n s + \omega_n^2}{s^2 + 2\zeta\omega_n s + \omega_n^2}$$

With:

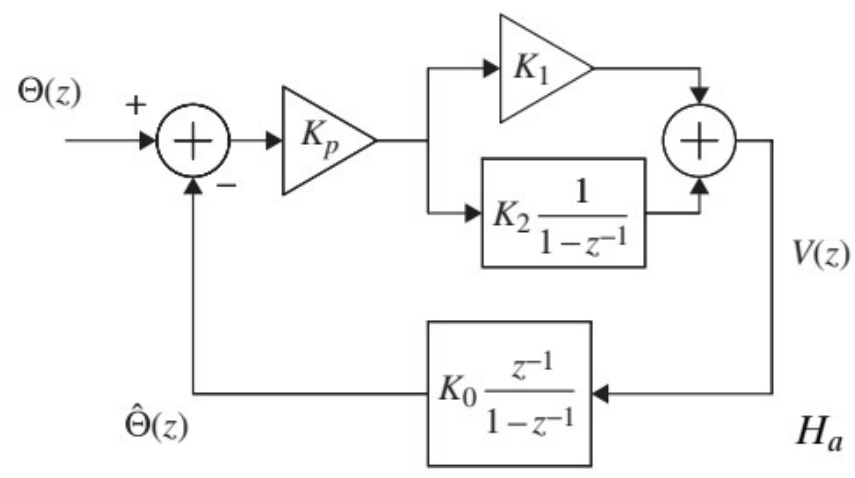
$$\zeta = \frac{k_1}{2} \sqrt{\frac{k_0 k_p}{k_2}} \quad \omega_n = \sqrt{k_0 k_p k_2}$$

PLL BW: $\omega_{3dB} = \omega_n \sqrt{1 + 2\zeta^2 + \sqrt{(1 + 2\zeta^2)^2 + 1}}$

PLL noise BW: $B_n = \frac{\omega_n}{2} \left(\zeta + \frac{1}{4\zeta} \right)$

2. QPSK modem: the main building blocks

- From analog PLL to digital PLL and its parameters
- We will restrict to a second order loop (the most used).
- The digital PLL (apply Tustin's equation)



$$H_d(z) = \frac{K_p K_0 (K_1 + K_2) z^{-1} - K_p K_0 K_1 z^{-2}}{1 - 2 \left(1 - \frac{1}{2} K_p K_0 (K_1 + K_2)\right) z^{-1} + (1 - K_p K_0 K_1) z^{-2}}$$

$$H_a \left(\frac{2}{T} \frac{1 - z^{-1}}{1 + z^{-1}} \right) = \frac{\frac{2\zeta\theta_n + \theta_n^2}{1 + 2\zeta\theta_n + \theta_n^2} + 2 \frac{\theta_n^2 - \zeta\theta_n}{1 + 2\zeta\theta_n + \theta_n^2} z^{-1} + \frac{\theta_n^2}{1 + 2\zeta\theta_n + \theta_n^2} z^{-2}}{1 - 2 \frac{\theta_n^2 - 1}{1 + 2\zeta\theta_n + \theta_n^2} z^{-1} + \frac{1 - 2\zeta\theta_n + \theta_n^2}{1 + 2\zeta\theta_n + \theta_n^2} z^{-2}}$$

Equating the denominator polynomials in Hd and Ha gives :

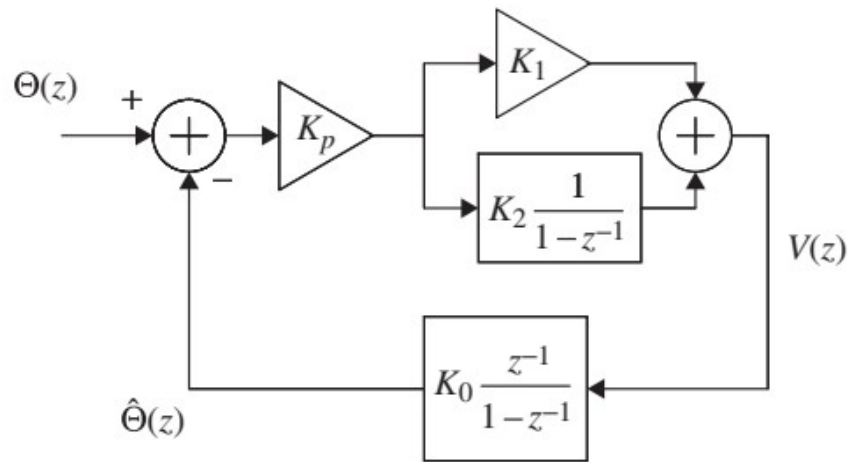
$$K_p K_0 K_1 = \frac{4\zeta\theta_n}{1 + 2\zeta\theta_n + \theta_n^2}$$

$$K_p K_0 K_2 = \frac{4\theta_n^2}{1 + 2\zeta\theta_n + \theta_n^2}$$

2. QPSK modem: the main building blocks

□ From analog PLL to digital PLL and its parameters

- We will restrict to a second order loop (the most used).
- The digital PLL (apply Tustin's equation)



With $N = T_s/T$ we finally get:

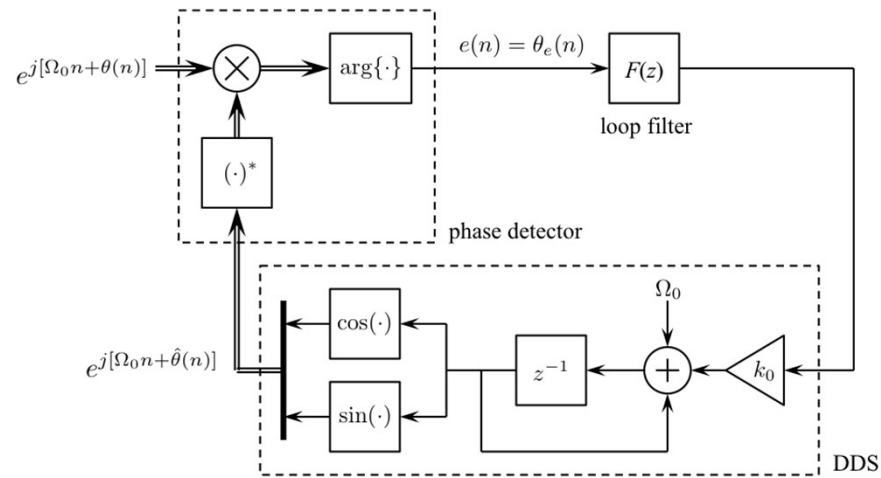
$$\theta_n = \frac{B_n T_s}{N \left(\zeta + \frac{1}{4\zeta} \right)}.$$

$$K_0 K_p K_1 = \frac{\frac{4\zeta}{N} \left(\frac{B_n T_s}{\zeta + \frac{1}{4\zeta}} \right)}{1 + \frac{2\zeta}{N} \left(\frac{B_n T_s}{\zeta + \frac{1}{4\zeta}} \right) + \left(\frac{B_n T_s}{N \left(\zeta + \frac{1}{4\zeta} \right)} \right)^2}$$

$$K_0 K_p K_2 = \frac{\frac{4}{N^2} \left(\frac{B_n T_s}{\zeta + \frac{1}{4\zeta}} \right)^2}{1 + \frac{2\zeta}{N} \left(\frac{B_n T_s}{\zeta + \frac{1}{4\zeta}} \right) + \left(\frac{B_n T_s}{N \left(\zeta + \frac{1}{4\zeta} \right)} \right)^2}$$

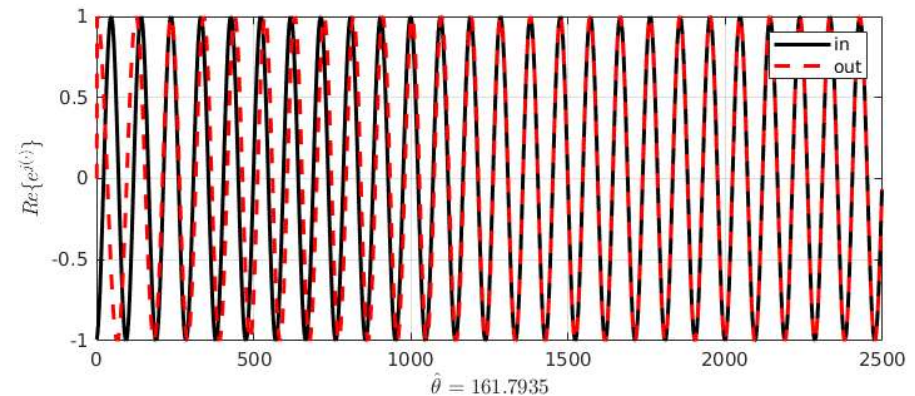
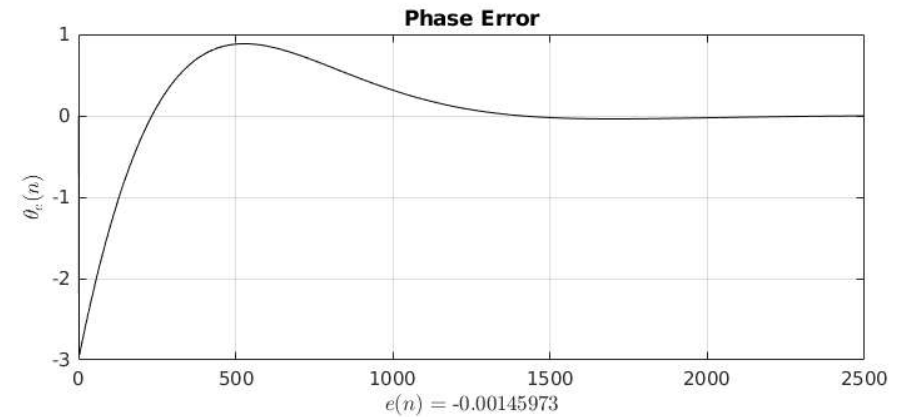
2. QPSK modem: the main building blocks

- From analog PLL to digital PLL and its parameters
- Digital PLL example



$$f_{\text{DDS}} = 0.01 \text{ cycles/sample}, f_{\text{in}} = 0.0105 \text{ cycles/sample}$$

$$\zeta = 0.707, B_n T = 0.2\%$$



We get: $K1 = 0.0053$
and $K2 = 1.4184e-05$

Outline

1 -

2 -

3 - The fully digital QPSK synchronizer.

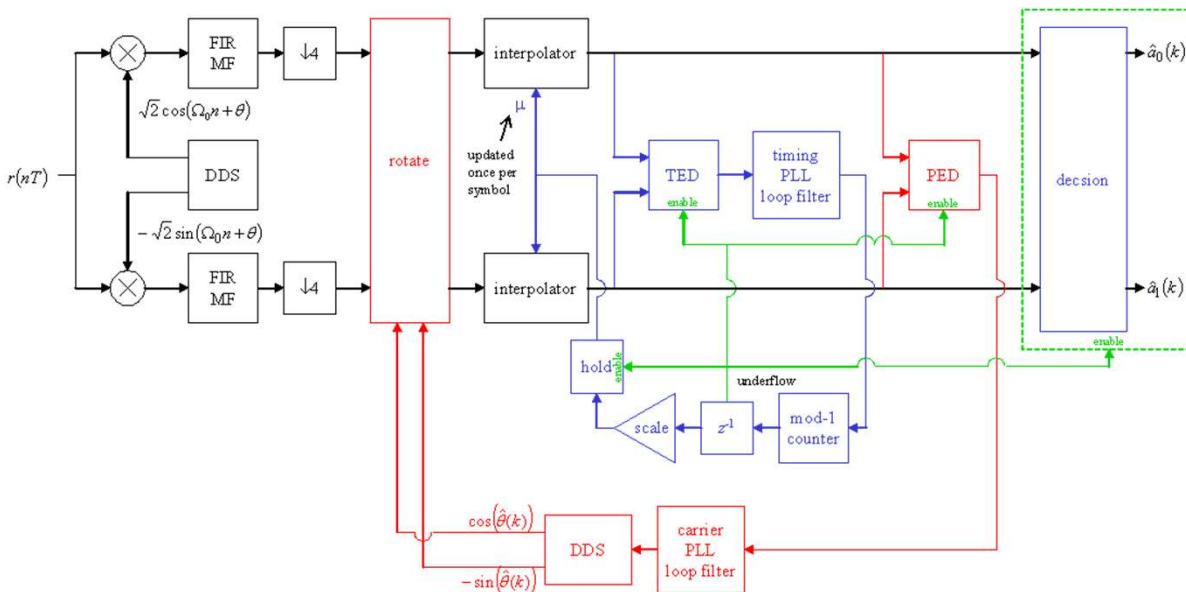
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3. The fully digital QPSK synchronizer

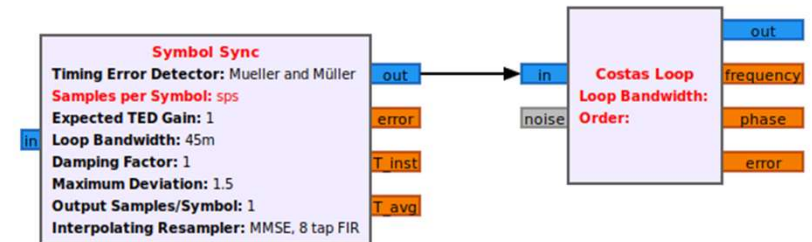
□ The all digital phase/frequency and timing synchronizer

What we want to build



The red parts = GNU Radio Costas Loop block

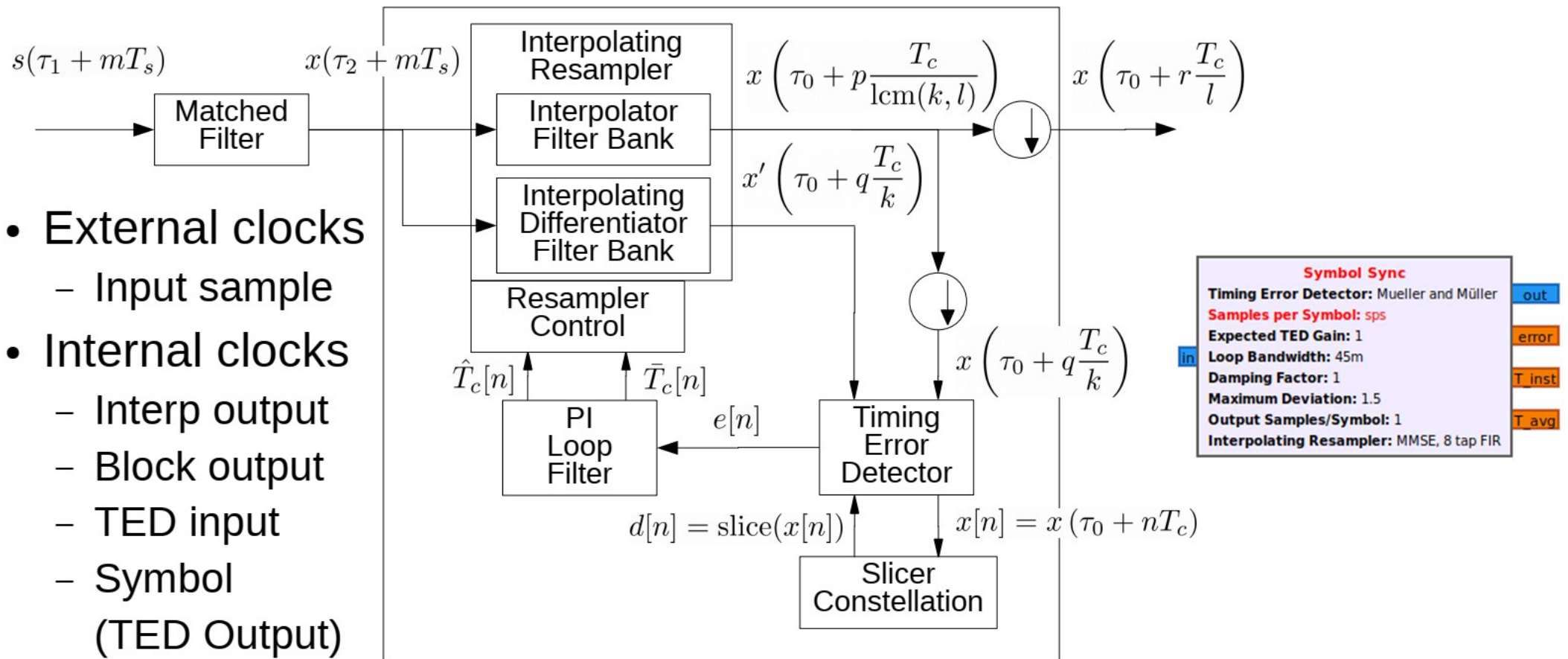
Has it something to do with this?



□ Let's concentrate on the symbol timing synchronization

3. The fully digital QPSK synchronizer

□ The timing synchronizer and A. Wall's GNU Radio Symbol Sync block



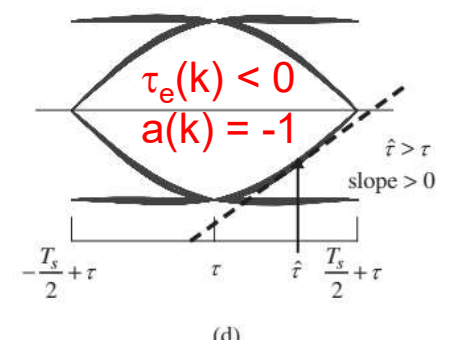
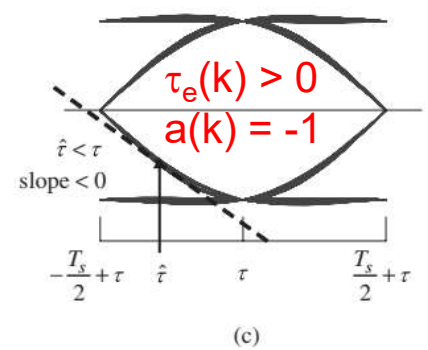
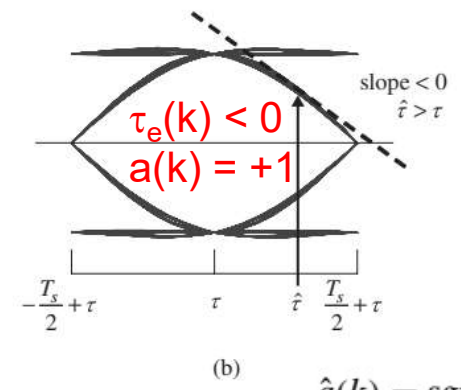
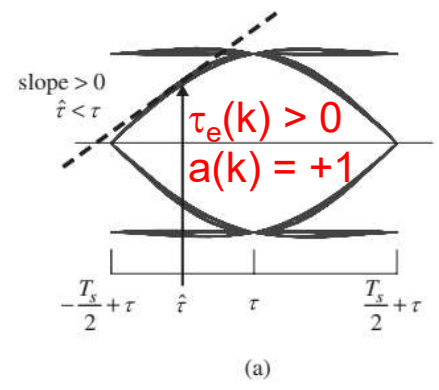
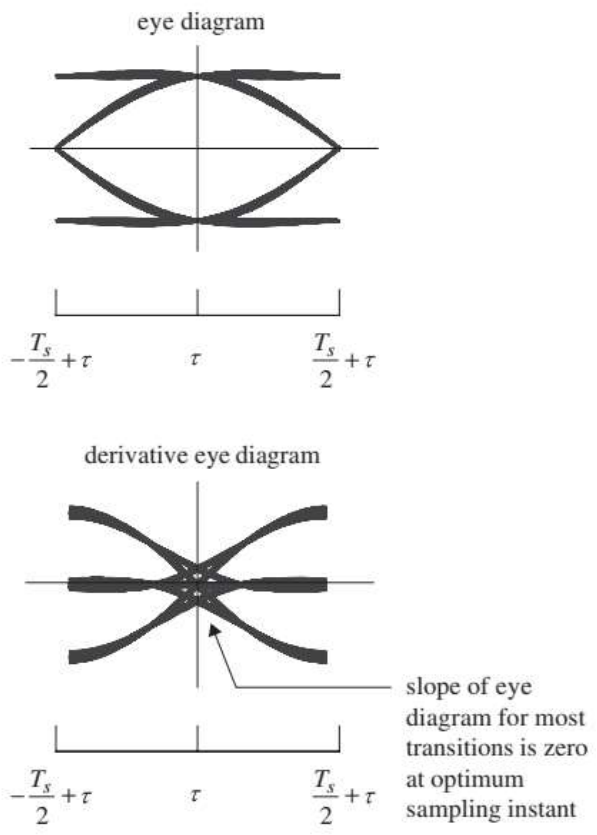
- External clocks
 - Input sample
- Internal clocks
 - Interp output
 - Block output
 - TED input
 - Symbol (TED Output)

➔ Two new elements: Interpolator and Timing Error Detector (TED)

3. The fully digital QPSK synchronizer

□ The timing synchronizer: Timing Error Detector (TED)

- Plays the role of phase detector in the DPLL
- Best understood with the eye diagram whose slope can be used to generate a timing error $e(k)$ (binary PAM)



$$\hat{a}(k) = \text{sgn} \{x(kT_s + \hat{t})\}$$

➔ Error signal:
ML estimate

$$e(k) = a(k)\dot{x}(kT_s + \hat{t}(k)) \quad \text{DA}$$

$$e(k) = \hat{a}(k)\dot{x}(kT_s + \hat{t}(k)) \quad \text{DD}$$

3. The fully digital QPSK synchronizer

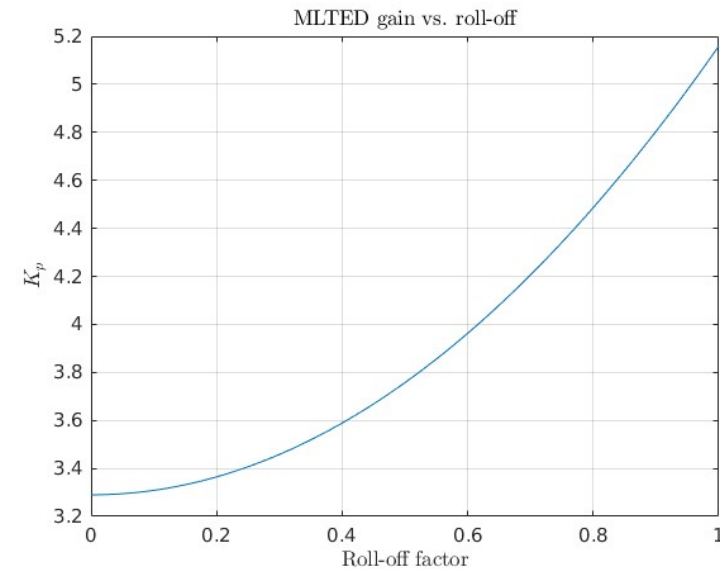
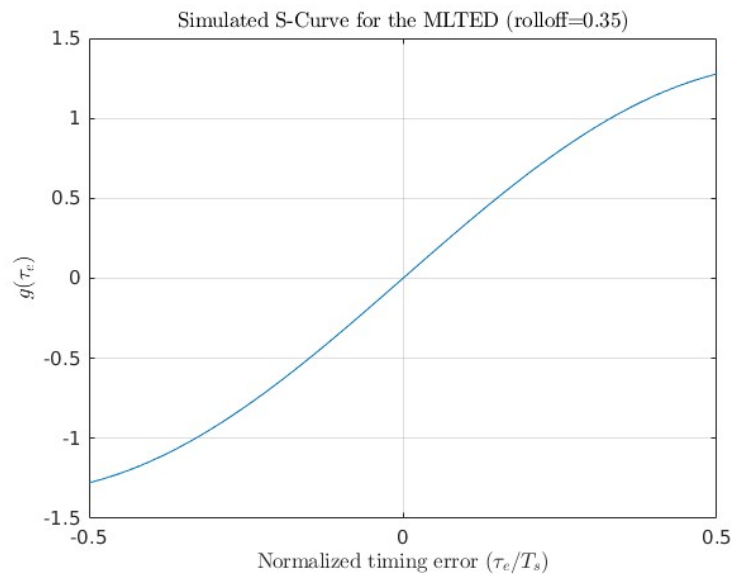
□ The timing synchronizer: Timing Error Detector (TED)

- There exists quite a lot of TED structures (ZC, M&M, Gardner etc.).
- Characteristics of TED described by the S-curve $g(\tau_e)$
- S-curve obtained by computing expected value of error signal:

$$g(\tau_e) = E\{e(k)\}$$

- For example for the MLTED we get:

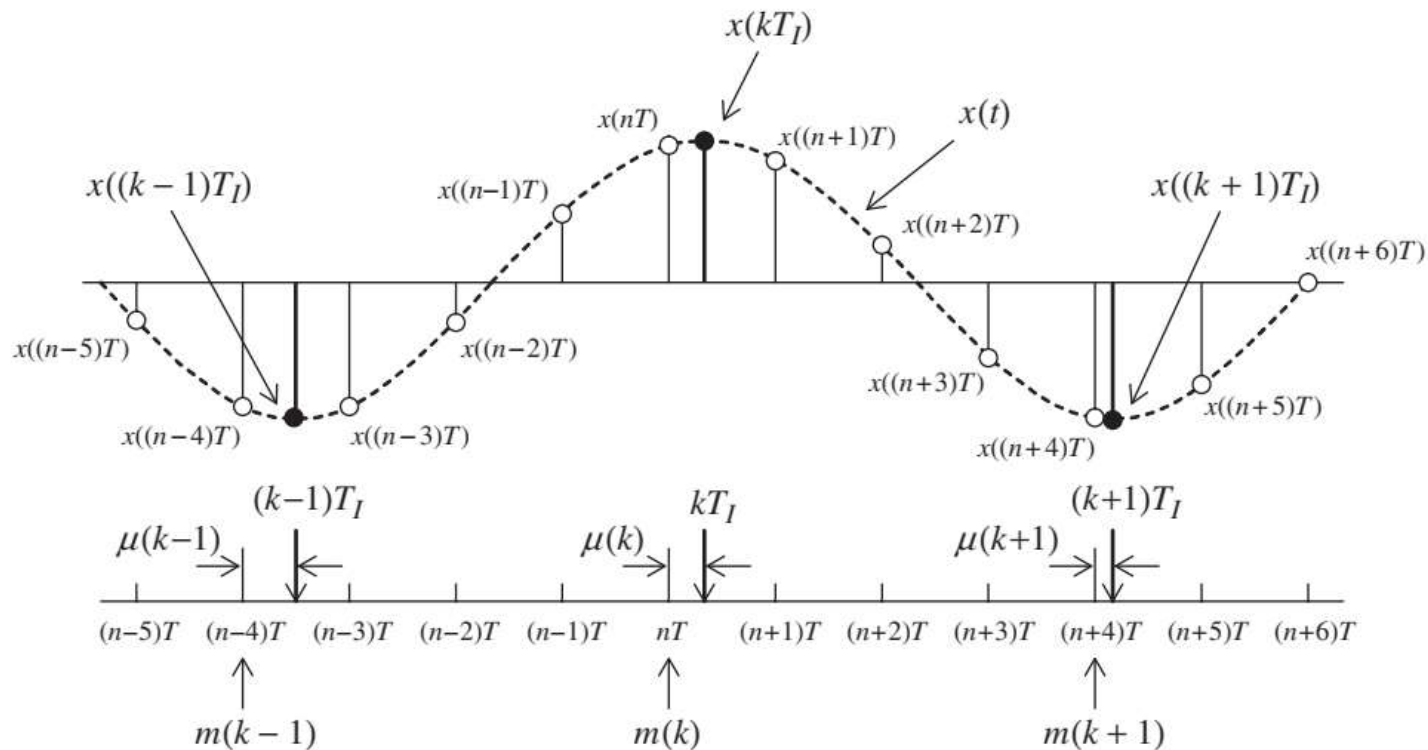
Needed by Symbol
Sync block!



3. The fully digital QPSK synchronizer

□ The timing synchronizer: Interpolator structures

- Because we use asynchronous sampling (i.e. sample clock independent to the data clock used at the transmitter) we need an interpolator.
- Some vocabulary:



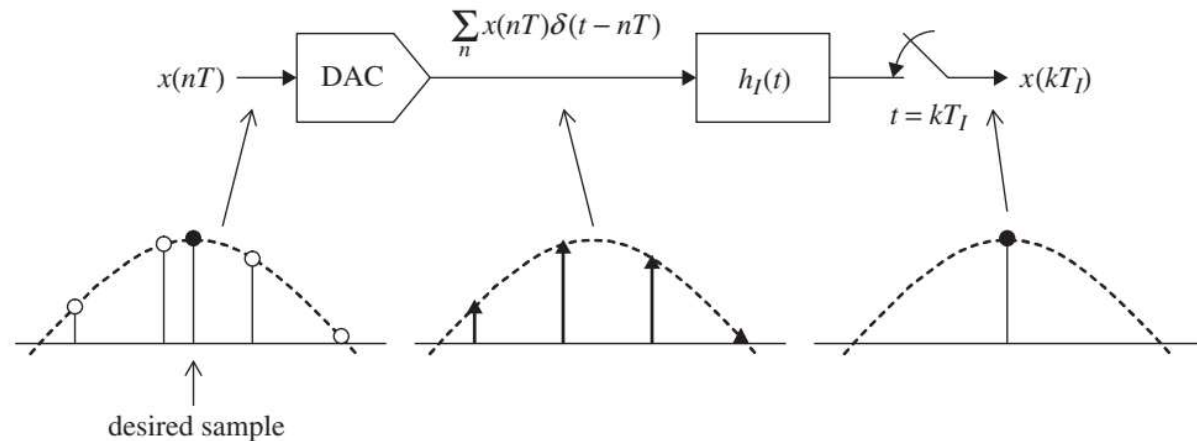
- k -th interpolant = kT_I
- When k -th *interpolant* is between samples $x(nT)$ and $x((n+1)T)$ the sample index n is called the k -th *basepoint index* and denoted $m(k)$.
- kT_I is some fraction of a sample time greater than $m(k)T$.
- This fraction is called the k -th fractional interval and is denoted $\mu(k)$. $0 < \mu(k) < 1$.
- It is defined by:

$$\mu(k)T = kT_I - m(k)T$$

3. The fully digital QPSK synchronizer

□ The timing synchronizer: Interpolator structures

- Conceptually, an interpolator can be seen as a filter.



- The k -th interpolant evaluated at $t = kT_I$, and may be expressed as:

$$x(kT_I) = \sum_n x(nT)h_I(kT_I - nT).$$

- If we reexpress with a filter index i , $m(k) = \text{int}(kT_I/T)$ and $\mu(k) = kT_I/T - m(k)$ the filter index is $i = m(k) - n$. Then:

$$x(kT_I) = \sum_i x((m(k) - i)T)h_I((i + \mu(k))T).$$

3. The fully digital QPSK synchronizer

□ The timing synchronizer: Interpolator structures

- From now to build the interpolator we can:
 - Use a FIR piecewise polynomial filter
 - A polyphase-filterbank (massively upsample input of matched filter then downsample matched filter output at an appropriately chosen sample offset to get desired interpolant).
- Let's have a look at the first possibility.
- The continuous underlying waveform is approximated by a polynomial of the form:

$$x(t) \approx c_p t^p + c_{p-1} t^{p-1} + \dots + c_1 t + c_0.$$

- The polynomial coefficient are determined by the $p + 1$ sample values surrounding the basepoint index. Once the coefficients values are known, the interpolant at $t = kT_I = (m(k) + \mu(k)T)$ is obtained by:

$$x(kT_I) \approx c_p (kT_I)^p + c_{p-1} (kT_I)^{p-1} + \dots + c_1 (kT_I) + c_0.$$

3. The fully digital QPSK synchronizer

□ The timing synchronizer: Interpolator structures

- Let's have a look at the first possibility.
- It can be shown that:

$$x((m(k) + \mu(k))T) = \sum_{i=-2}^1 h_2(i)x((m(k) - i)T)$$

- In the case of a parabolic interpolator this leads to four coefficients:

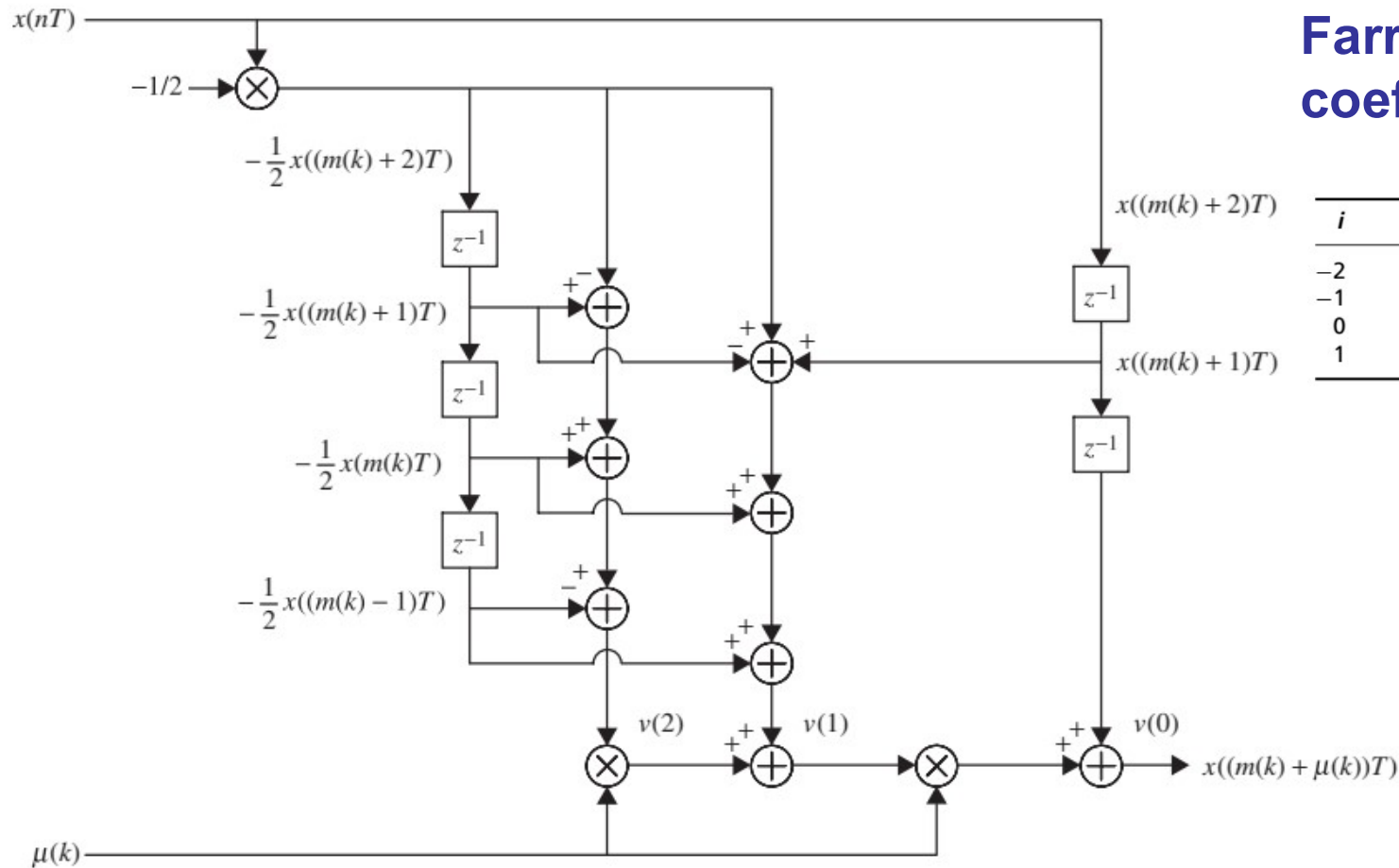
$$\begin{cases} h_I[-2 + \mu_k] = \alpha\mu_k^2 - \alpha\mu_k \\ h_I[-1 + \mu_k] = -\alpha\mu_k^2 + (\alpha + 1)\mu_k \\ h_I[\mu_k] = -\alpha\mu_k^2 + (\alpha - 1)\mu_k + 1 \\ h_I[1 + \mu_k] = \alpha\mu_k^2 - \alpha\mu_k \end{cases}$$

- The interpolation equation becomes:

$$\begin{aligned} y(\mu_k) &= \sum_{i=-2}^1 x[(-i)]h_I[(i + \mu_k)] \\ &= x[2](\alpha\mu_k^2 - \alpha\mu_k) + x[1](-\alpha\mu_k^2 + (\alpha + 1)\mu_k) \\ &\quad + x[0](-\alpha\mu_k^2 + (\alpha - 1)\mu_k + 1) + x[-1](\alpha\mu_k^2 - \alpha\mu_k) \end{aligned}$$

3. The fully digital QPSK synchronizer

□ The timing synchronizer: Interpolator structures



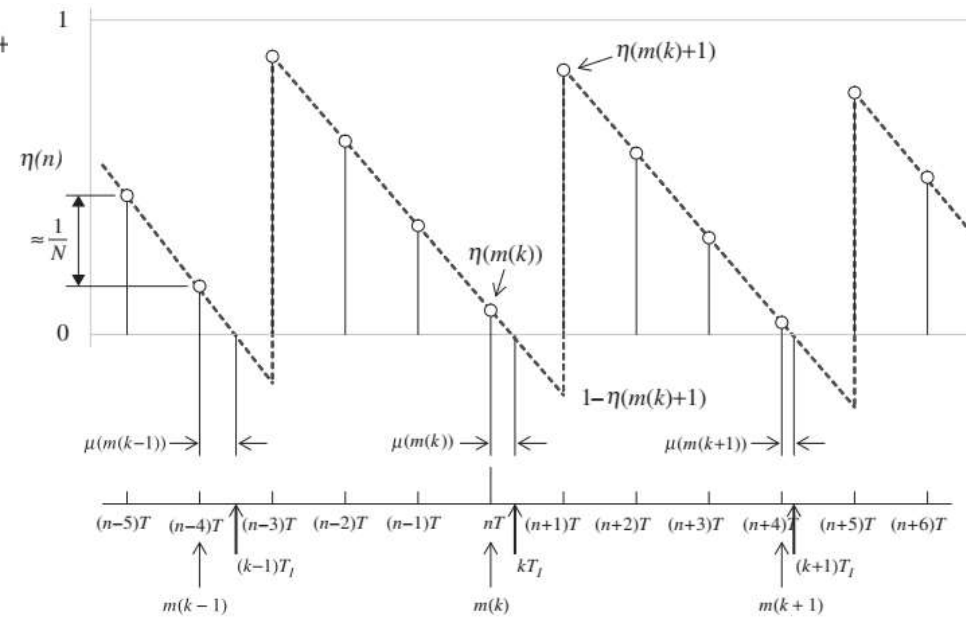
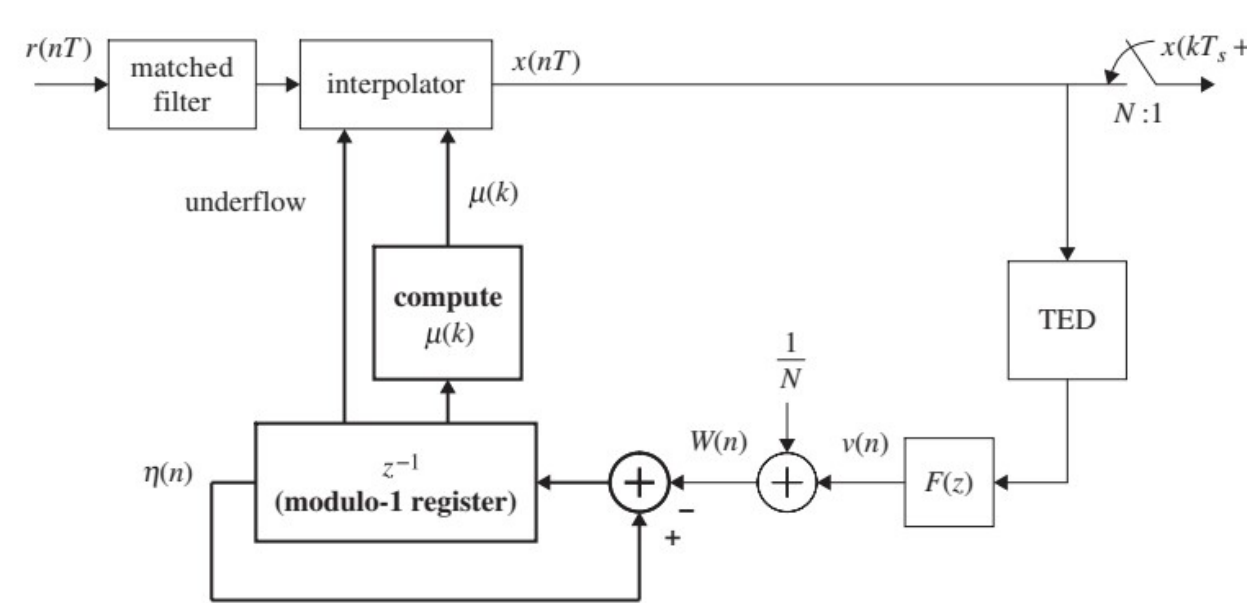
Farrow filter coefficients:

i	$b_2(i)$	$b_1(i)$	$b_0(i)$
-2	α	$-\alpha$	0
-1	$-\alpha$	$1 + \alpha$	0
0	$-\alpha$	$\alpha - 1$	1
1	α	$-\alpha$	0

3. The fully digital QPSK synchronizer

□ The timing synchronizer: Interpolator structures

- The Farrow interpolator is controlled by a modulo 1 counter:



Outline

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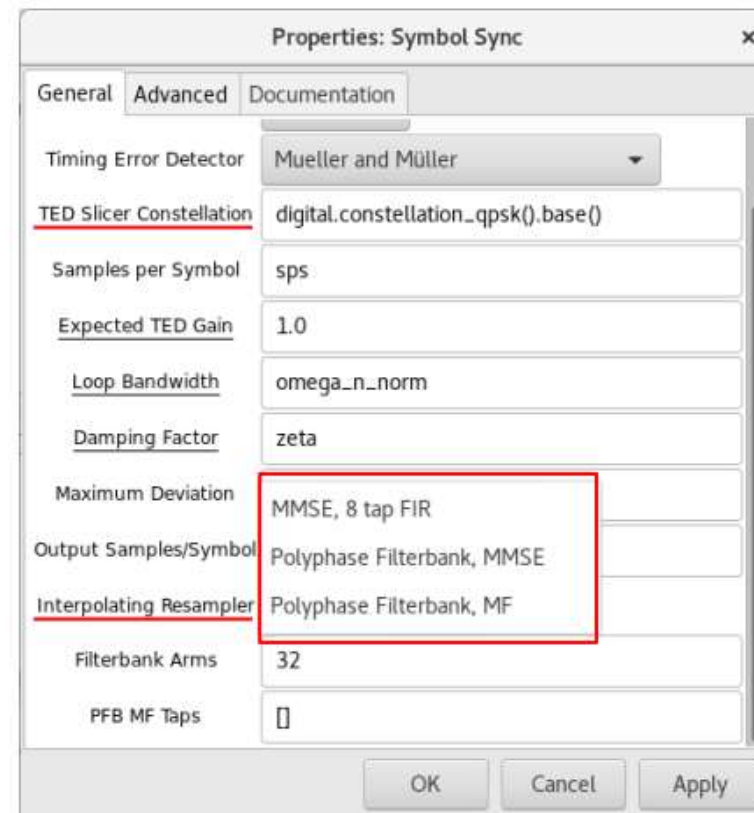
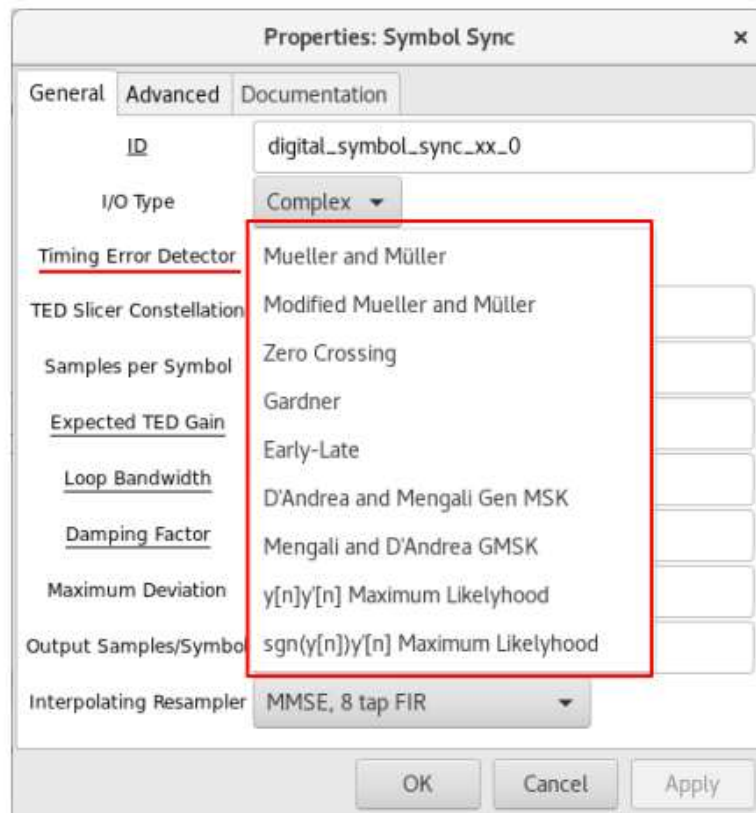
3 -

4 - GNU Radio demo with real hardware

5 -

4. GNU Radio demo with real hardware

□ QPSK system with the Adalm-Pluto



Outline

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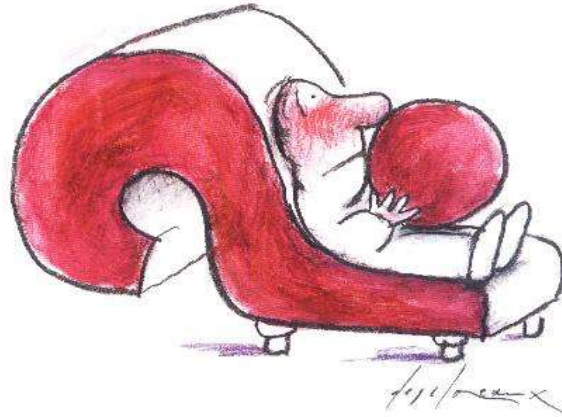
5 - Conclusion

5. Conclusion

- ❑ **Going from simulation to implementation adds (a lot of) complexity.**
- ❑ **Digital synchronization functions understanding and implementation require a good level in digital signal processing.**
- ❑ **Practical implementations are requested by today's students.**
- ❑ **For this particular purpose, GNU Radio is the right tool!**

- [1] M. Rice, “Digital Communications: a discrete time approach”, 2nd Edition, Author, 2020.
- [2] T. P. Zielinski, “Starting Digital Signal Processing in Telecommunication Engineering”, Springer, 2021.
- [3] <https://igorfreire.com.br/2016/10/15/symbol-timing-synchronization-tutorial/>
- [4] <http://ricesimulink.groups.et.byu.net/>

Thank you for your attention!



Questions?